International Symposium on Modelling of exhaust-gas after-treatment



Development of a SCR System for a Dual Line Exhaust by Using Two-Phase Flow CFD Calculations

Bernd Amon, Herbert Albert, Faurecia Johann Wurzenberger, Moritz Frobenius, AVL





- Motivation
- Analysis of the Basic Design of the Exhaust System
- Applied CFD Methods
- Test bed Verification
- Conclusions

CONTENT



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EMISSION LIMITS – LDV DIESEL





Vehicle weight



SCR SYSTEM







• To receive a high reduction rate on NOx by the SCR catalyst a very good distribution of the reducing agent on the catalyst surface is necessary



Starting Design

- Dual pipe
- 2 SCR catalysts
- Flex pipe in front of catalyst
- No location for injection



Optimized Packaging

- Location for injection optimized
- 1 SCR catalyst with optimized geometry
- Optimized outlet cone

Basic design

F u A

Find concept to use only <u>one</u> AdBlue injection

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Development Concept

- Lean use simulation/ prediction
- Only final validation on engine test bench

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AdBlue injection in two pipes (basic 2)

ANALYSIS OF "BEST vs. WORST CASE" CFD Simulation - Results

AdBlue injection in one pipe (basic 1)



- With one AdBlue injection valve the ammonia distribution on the catalyst surface is not sufficient (left)
- With two AdBlue injection valves the CFD calculation shows a better uniformity of ammonia (right), but at higher costs

DESIGN OPTIMIZATION AND VALIDATION **faurecia**

Swirl Cone Design



CFD-calculations (single-phase, steady state)



Distribution of passive scalar



0500





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CFD-SCR-SIMULATION

Fluid Properties and Multi-component evaporation and thermoysis





Temperature and composition dependent modelling of

- liquid density, viscosity, specific heat
- solution vapour pressure

Properties for gaseous urea

- vapour heat capacity
- vapour dynamic viscosity

Spray / gas phase

- multi-component evaporation
- thermolysis
- hydrolysis



CFD-SCR-SIMULATION Spray and Wallfilm modelling



FIRE[®]

Advanced Spray-Wall Modells

- Multicomponent wallfilm evaporation and thermolysis
- Modelling of heat transfer between droplets and wall (Wruck-Meingast)
- Wall temperatur dependent splashing model (Kuhnke with Birkhold Extension)
- Accounting for heat conduction in solid walls via lateral heat conduction

D. Kuhnke. Spray Wall Interaction Modelling by Dimensionless Data Analysis. PhD thesis, TU Darmstadt 2004.N. W. Wruck. Transientes Sieden von Tropfen beim Wandaufprall. PhD thesis, RWTH Aachen, 1998.



CFD-SCR-SIMULATION Model validation



Schwarzenberg, M. Untersuchung von Spraykonzepten zur Dosierung von Harnstoff-Wasser-Lösung beim Einsatz eines SCR-Verfahrens. Diplomarbeit, RWTH Aachen, 2005

F. Birkhold, U. Meingast, P. Wassermann, O. Deutschmann. Modeling and simulation of the injection of urea-water-solution for automotive SCR DeNOx-systems. Applied Catalyst B 70 (2007), 119-127



CFD-SCR-SIMULATION Energy

Simulation



Heat conductivity

Single wall tube	$s/\lambda = 6.10^{-5} (m^2 K)/W$
Decoupling element	$s/\lambda = 7.5 \cdot 10^{-2} (m^2 K)/W$
Flange	$s/\lambda = 5.10^{-2} (m^2 K)/W$
Converter cover	$s/\lambda = 3.55 \cdot 10^{-2} \text{ (m}^2\text{K)/W}$
Cones	$s/\lambda = 8.10^{-5} (m^2 K)/W$

Heat transfer outside $\alpha_a = 10 \text{ W/(m^2K)}$

Thermo camera



Radiation

Emission coeff $\varepsilon = 0.5$ @ 30 °C



CFD-SCR-SIMULATION Meshing





CFD-SCR-SIMULATION Results

Swirl Design Basic_EOP_B4:TI_1.1:Wallfilm:Thickness[m] Swirl_EOP_B4:TI_1.1:Wallfilm:Thickness[m] 1.5e-05 1.5e-05 Basic EOP B4:TI 1.1:Species:Mole Fraction HCNO[-] 30-05 Swirl EOP B4:TI 1.1:Species:Mole Fraction HCNO[-] 30-05 0.0015 0.0015 Ref 7 Ref 7 0.001125 0.001125 0 00075 0.00075 Basic_EOP_B4:TI_1.1:Species:Mole_Fraction_NO[-] Swirl_EOP_B4:TI_1.1:Species:Mole_Fraction_NO[-] 0.00043847 0.000375 0.000375 0.00032885 0.00032885 0.00021923 0.00021923 0.00010962 0.00010962 Basic_EOP_B4:TI_1.1:Species:Mole_Fraction_NH3[-] Basic_EOP_B4:TI_1.1:Species:Mole_Fraction_NO2[-] Swirl_EOP_B4:TI_1.1:Species:Mole_Fraction_NH3[-] Swirl_EOP_B4:TI_1.1:Species:Mole_Fraction_NO2[-] 0.0015 Ref 7x 0.0015 Ref 7x Bef 8 0.001125 0.00014173 0.001125 0.00014173 0.00075 9.4487e-05 0.00075 9.4487e-05 0.000375 4.7244e-05 0.000375 4.7244e-05 Basic_EOP_B4:TI_1.1:SprayDroplet:ParcelMass[kg] Swirt_EOP_B4:TI_1.1:SprayDroplet:ParcelMass[kg] 10.02 \odot 0 (8x ଡ଼ୄୄୠୄୄୄୄ

OP B

Basic Design

MODEGAT, 15. September 2009

7x

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ENGINE TEST BENCH INVESTIGATIONS







Engine: Max. power: Max torque:

Diesel V8, 4.2 ltr, turbocharged 240 kW @ 3750 rpm 760 Nm @ 1800...2500 rpm

Operating Points:

Operating point (OP)		А	В
Speed	[rpm]	1700	3200
Load	[Nm]	160	390
Mass Intake Air	[kg/h]	136	700
T before SCR	[°C]	300	450







Swirl



ENGINE TEST BENCH SET-UP





NOx DISTRIBUTION MEASUREMENTS

Gas divider

Mapping: 48 NO_x + NH_3 sampling points



$$\gamma = 1 - \frac{\sum_{i=1}^{|c_i - c_i|}}{2n\overline{c}}$$

NOx DISTRIBUTION MEASUREMENTS Results







CFD-SCR-SIMULATION

Results basic design- comparison with engine bench











CFD-SCR-SIMULATION Results swirl design-comparison with engine bench







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- Advanced CFD models for ad-blue sprays and spray-wall interaction have been applied → accurate prediction of NH3-uniformity in good correlation with test bed results
- Successful development of a high performance SCR system for a dual line exhaust system (V8-engine) → Swirl cone design allows a high performance of the SCR catalytic converter
- In such exhaust system only one AdBlue injection is necessary to achieve a sufficient ammonia distribution on the SCR catalyst → Reduction of system costs and complexity of SCR control
- The application of accurate simulation-tools enables a fast and costeffective virtual system development

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